



U.S. NUCLEAR REGULATORY COMMISSION  
**STANDARD REVIEW PLAN**

**BRANCH TECHNICAL POSITION 3-4**

**POSTULATED RUPTURE LOCATIONS IN FLUID SYSTEM PIPING INSIDE AND OUTSIDE CONTAINMENT**

**REVIEW RESPONSIBILITIES**

**Primary** - Organization responsible for Mechanical Engineering reviews

**Secondary** - None

**A. BACKGROUND**

This position on pipe rupture postulation is intended to comply with the requirements of 10 CFR Part 50, Appendix A, General Design Criteria (GDC) 4 for the design of nuclear power plant structures, systems and components (SSCs). It is recognized that pipe rupture is a rare event that may only occur under unanticipated conditions, such as those which might be caused by possible design, construction, or operation errors; unanticipated loads; or unanticipated corrosive environments. The staff's observation of actual piping failures has indicated that they generally occur at high stress and fatigue locations, such as at the terminal ends of a piping system at its connection to the nozzles of a component. The criteria of this position are intended to utilize the available piping design information by postulating pipe ruptures at locations having relatively higher potential for failure, such that an adequate and practical level of protection may be achieved.

Subject to certain limitations, GDC 4 allows dynamic effects associated with postulated pipe ruptures to be excluded from the design basis when analyses reviewed and approved by the

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**USNRC STANDARD REVIEW PLAN**

This Standard Review Plan, NUREG-0800, has been prepared to establish criteria that the U.S. Nuclear Regulatory Commission staff responsible for the review of applications to construct and operate nuclear power plants intends to use in evaluating whether an applicant/licensee meets the NRC's regulations. The Standard Review Plan is not a substitute for the NRC's regulations, and compliance with it is not required. However, an applicant is required to identify differences between the design features, analytical techniques, and procedural measures proposed for its facility and the SRP acceptance criteria and evaluate how the proposed alternatives to the SRP acceptance criteria provide an acceptable method of complying with the NRC regulations.

The standard review plan sections are numbered in accordance with corresponding sections in Regulatory Guide 1.70, "Standard Format and Content of Safety Analysis Reports for Nuclear Power Plants (LWR Edition)." Not all sections of Regulatory Guide 1.70 have a corresponding review plan section. The SRP sections applicable to a combined license application for a new light-water reactor (LWR) are based on Regulatory Guide 1.206, "Combined License Applications for Nuclear Power Plants (LWR Edition)."

These documents are made available to the public as part of the NRC's policy to inform the nuclear industry and the general public of regulatory procedures and policies. Individual sections of NUREG-0800 will be revised periodically, as appropriate, to accommodate comments and to reflect new information and experience. Comments may be submitted electronically by email to [NRR\\_SRP@nrc.gov](mailto:NRR_SRP@nrc.gov).

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Commission demonstrate that the probability of fluid system piping rupture is extremely low under design basis conditions. These analyses are commonly referred to as “leak-before-break” (LBB) analyses. The application of LBB to piping system design is reviewed in accordance with SRP Section 3.6.3.

In the ABWR and System 80+ design certification FSERs, the staff accepted an exemption to 10 CFR 100, Appendix A that the design of all safety-related SSCs consider operating basis earthquake (OBE) loads. In SECY 93-087, the staff recommended that the Commission approve the approach to eliminate the OBE from the design of SSCs.

Furthermore, the Staff concluded that no replacement earthquake loading should be used to establish the postulated pipe rupture and leakage crack locations once the OBE is eliminated from the design and that the criteria for postulating pipe ruptures and leakage cracks in high- and moderate-energy piping systems should be based on factors attributed only to normal and operational transients. However, for establishing pipe breaks and leakage cracks due to fatigue effects, the Staff concluded that calculation of the cumulative usage factor should continue to include seismic cyclic effects.

## **B. BRANCH TECHNICAL POSITION**

### **A. High-Energy Fluid Systems Piping**

- (i) Fluid Systems Separated From Essential Systems and Components. For the purpose of satisfying the separation provisions of plant arrangement as specified in B.1.a of Branch Technical Position (BTP) 3-3, a review of the piping layout and plant arrangement drawings should clearly show that the effects of postulated piping breaks at any location are isolated or are physically remote from essential systems and components.<sup>1</sup> At the designer's option, break locations as determined from 2A(iii) of this position may be assumed for this purpose.
  
- (ii) Fluid System Piping in Containment Penetration Areas. Breaks and cracks need not be postulated in those portions of piping from containment wall to and including the inboard or outboard isolation valves, provided they meet the design criteria of the ASME Code, Section III, Subarticle NE-1120, and the following additional design criteria:
  - (1) The following design stress and fatigue limits should not be exceeded:  
For ASME Code, Section III, Class 1 Piping
    - (a) The maximum stress range between any two load sets (including the zero load set) should not exceed  $2.4 S_m$  and should be calculated<sup>2</sup> by Eq. (10) in ASME Code, Section III, NB-3653.

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<sup>1</sup> Systems and components necessary to shut down the reactor and mitigate the consequences of a postulated pipe rupture without offsite power.

<sup>2</sup> For those loads and conditions for which Level A and Level B stress limits have been specified in the design specification (including the operating basis earthquake).

If the calculated maximum stress range of Eq. (10) exceeds  $2.4 S_m$ , the stress ranges calculated by both Eq. (12) and Eq. (13) in Paragraph ASME Code, Section III, NB-3653 should meet the limit of  $2.4 S_m$ .

- (b) The cumulative usage factor should be less than 0.1.
- (c) The maximum stress, as calculated by Eq. (9) in ASME Code, Section III, NB-3652 under the loadings resulting from a postulated piping failure beyond these portions of piping, should not exceed  $2.25 S_m$  and  $1.8 S_y$ , except that following a failure outside containment, the pipe between the outboard isolation valve and the first restraint may be permitted higher stresses provided a plastic hinge is not formed and operability of the valves with such stresses is ensured in accordance with the criteria specified in SRP Section 3.9.3. Primary loads include those which are deflection-limited by whip restraints.

For ASME Code, Section III, Class 2 Piping

- (d) The maximum stress ranges as calculated by the sum of Eqs.(9) and (10) in Paragraph NC-3653, ASME Code, Section III, considering those loads and conditions thereof for which level A and level B stress limits have been specified in the system's design specification (i.e., sustained loads, occasional loads, and thermal expansion), including an OBE event (if applicable), should not exceed  $0.8(1.8 S_h + S_A)$ . The  $S_h$  and  $S_A$  are allowable stresses at maximum (hot) temperature and allowable stress range for thermal expansion, respectively, as defined in Article NC-3600 of the ASME Code, Section III.
- (e) The maximum stress, as calculated by ASME Code, Section III, NC-3653, paragraph Eq. (9) under the loadings resulting from a postulated piping failure of fluid system piping beyond these portions of piping, should not exceed  $2.25 S_h$  and  $1.8 S_y$ .

Primary loads include those which are deflection-limited by whip restraints. The exceptions permitted in (c) above may also be applied, provided that when the piping between the outboard isolation valve and the restraint is constructed in accordance with the Power Piping Code ANSI B31.1, the piping should either be of seamless construction with full radiography of all circumferential welds or all longitudinal and circumferential welds should be fully radiographed.

- (2) Welded attachments, for pipe supports or other purposes, to these portions of piping should be avoided, except where detailed stress analyses, or tests, are performed to demonstrate compliance with the limits of 2.A(ii)(1).
- (3) The number of circumferential and longitudinal piping welds and branch connections should be minimized. Where guard pipes are used, the

enclosed portion of fluid system piping should be seamless construction and without circumferential welds unless specific access provisions are made to permit inservice volumetric examination of the longitudinal and circumferential welds.

- (4) The length of these portions of piping should be reduced to the minimum length practical.
- (5) The design of pipe anchors or restraints (e.g., connections to containment penetrations and pipe-whip restraints) should not need welding directly to the outer surface of the piping (e.g., flued integrally forged pipe fittings may be used), except where such welds are 100% volumetrically examinable in service and a detailed stress analysis is performed to demonstrate compliance with the limits of 2.A(ii)(1).
- (6) Guard pipes provided for those portions of piping in the containment penetration areas should be constructed in accordance with the criteria of the ASME Code, Section III, Subsection NE, Class MC, where the guard pipe is part of the containment boundary. In addition, the entire guard pipe assembly should be designed to meet the following criteria and tests:
  - (a) The design pressure and temperature should not be less than the maximum operating pressure and temperature of the enclosed pipe under normal plant conditions.
  - (b) The Level C stress limits in, ASME Code, Section III, NE-3220 should not be exceeded under the loading associated with containment design pressure and temperature in combination with the safe shutdown earthquake.
  - (c) Guard pipe assemblies should be subjected to a single pressure test at a pressure not less than its design pressure.
  - (d) Guard pipe assemblies should not prevent the access necessary to conduct the inservice examination specified in 2.A(ii)(7). Inspection ports, if used, should not be located in that portion of the guard pipe through the annulus of dual barrier containment structures.
- (7) A 100% volumetric inservice examination of all pipe welds should be conducted during each inspection interval as defined in ASME Code, Section XI, IWA-2400.

(iii) Postulation of Pipe Breaks in Areas Other Than Containment Penetration

- (1) With the exceptions of those portions of piping identified in 2.A(ii), breaks in Class 1 piping (ASME Code, Section III) should be postulated at the following locations in each piping and branch run:

- (a) At terminal ends.<sup>3</sup>
- (b) At intermediate locations where the maximum stress range<sup>2</sup> as calculated by Eq. (10) and either Eq. (12) or Eq. (13) exceeds  $2.4 S_m$ .
- (c) At intermediate locations where the cumulative usage factor exceeds 0.1.

As a result of piping reanalysis, the highest stress locations may be shifted; however, the initially determined intermediate break locations need not be changed unless one of the following conditions exists:

- (i) The dynamic effects from the new (as-built) intermediate break locations are not mitigated by the original pipe-whip restraints and jet shields.
  - (ii) A change is necessary in pipe parameters such as major differences in pipe size, wall thickness, and routing.
- (2) With the exceptions of those portions of piping identified in 2A(ii), breaks in Class 2 and 3 piping (ASME Code, Section III) should be postulated at the following locations in those portions of each piping and branch run:
- (a) At terminal ends.
  - (b) At intermediate locations selected by one of the following criteria:
    - (i) At each pipe fitting (e.g., elbow, tee, cross, flange, and nonstandard fitting), welded attachment, and valve. Or, where the piping contains no fittings, welded attachments, or valves, at one location at each extreme of the piping run adjacent to the protective structure.
    - (ii) At each location where stresses are calculated<sup>2</sup> by the sum of Eqs. (9) and (10) in NC/ND-3653 of ASME Code, Section III, to exceed 0.8 times the sum of the stress limits given in NC/ND-3653.

As a result of piping reanalysis, due to differences between the design configuration and the as-built configuration, the highest stress locations may be shifted;

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<sup>3</sup> This is defined as the extremities of piping runs that connect to structures, components (e.g., vessels, pumps, valves), or pipe anchors that act as rigid constraints to piping motion and thermal expansion. A branch connection to a main piping run is a terminal end of the branch run, except where the branch run is classified as part of a main run in the stress analysis and is shown to have a significant effect on the main run behavior. In piping runs that are maintained pressurized during normal plant conditions for only a portion of the run (i.e., up to the first normally closed valve), a terminal end of such a run is the piping connection to this closed valve.

however, the initially determined intermediate break locations may be used unless redesign of the piping resulting in a change in pipe parameters (diameter, wall thickness, routing) is necessary, or the dynamic effects from the new (as-built) intermediate break locations are not mitigated by the original pipe-whip restraints and jet shields.

- (3) Breaks in seismically analyzed non-ASME Class piping are postulated according to the same criteria as for ASME Class 2 and 3 piping above.<sup>4</sup>
  - (4) Applicable to (1), (2), and (3) above:

If a structure separates a high-energy line from an essential component, that separating structure should be designed to withstand the consequences of the pipe break in the high-energy line which produces the greatest effect at the structure, irrespective of the fact that the above criteria might not need such a break location to be postulated.
  - (5) Safety-related equipment should be environmentally qualified in accordance with SRP Section 3.11. Appropriate pipe ruptures and leakage cracks (whichever controls) should be included in the design bases for environmental qualification of electrical and mechanical equipment both inside and outside the containment.
- (iv) The designer should identify each piping run it considered in order to postulate the break locations pursuant to 2.A(iii) above. In complex systems such as those containing arrangements of headers and parallel piping running between headers, the designer should identify and include all such piping within a designated run in order to postulate the number of breaks pursuant to these criteria.
  - (v) With the exceptions of those portions of piping identified in 2.A(ii), leakage cracks should be postulated as follows:
    - (1) For ASME Code, Section III, Class 1 piping, at axial locations where the calculated stress range<sup>2</sup> by Eq. (10) in NB-3653 exceeds 1.2 S(m).
    - (2) For ASME Code, Section III, Class 2 and 3 or nonsafety-class (not ASME Class 1, 2, or 3) piping, at axial locations where the calculated stress<sup>2</sup> by the sum of Eqs. (9) and (10) in NC/ND-3653 exceeds 0.4 times the sum of the stress limits given in NC/ND-3653.
    - (3) Nonsafety-class piping that has not been evaluated to obtain stress information should have leakage cracks postulated at axial locations that produce the most severe environmental effects.

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<sup>4</sup> Note that, in addition, breaks in nonseismic (i.e., non-Category I) piping should be taken into account as described in Section II.2.k, "Interaction of Other Piping with Category I Piping," of SRP Section 3.9.2.

B. Moderate-Energy Fluid System Piping

- (i) Fluid Systems Separated from Essential Systems and Components. For the purpose of satisfying the separation provisions of plant arrangement as specified in B.1.a of BTP 3-3, a review of the piping layout and plant arrangement drawings should clearly show that the effects of through-wall leakage cracks at any location in piping designed to seismic and nonseismic standards are isolated or physically remote from essential systems and components.
- (ii) Fluid System Piping in Containment Penetration Areas. Leakage cracks need not be postulated in those portions of piping from containment wall to and including the inboard or outboard isolation valves, provided 1) they meet the criteria of the ASME Code, Section III, NE-1120, and 2) the stresses calculated<sup>2</sup> by the sum of Eqs. (9) and (10) in ASME Code, Section III, NC-3653 do not exceed 0.4 times the sum of the stress limits given in NC-3653.
- (iii) Fluid Systems in Areas Other Than Containment Penetration.
  - (1) Leakage cracks should be postulated in piping located adjacent to structures, systems, or components important to safety, except:
    - (a) Where exempted by 2.B(ii) or 2.B(iv),
    - (b) For ASME Code, Section III, Class 1 piping, where the stress range calculated<sup>2</sup> by Eq. (10) in NB-3653 is less than 1.2 S(m), and
    - (c) For ASME Code, Section III, Class 2 or 3 and nonsafety-class piping, where the stresses calculated<sup>2</sup> by the sum of Eqs. (9) and (10) in NC/HD-3653 are less than 0.4 times the sum of the stress limits given in NC/ND-3653.
  - (2) Leakage cracks, unless the piping system is exempted by (1) above, should be postulated at axial and circumferential locations that result in the most severe environmental consequences.
  - (3) Leakage cracks should be postulated in fluid system piping designed to nonseismic standards as necessary to satisfy B.3.d of BTP 3-3.
- (iv) Moderate-Energy Fluid Systems in Proximity to High-Energy Fluid Systems. Leakage cracks need not be postulated in moderate-energy fluid system piping located in an area in which a break in high-energy fluid system piping is postulated, provided such leakage cracks would not result in more limiting environmental conditions than the high-energy piping break. Where a postulated leakage crack in the moderate-energy fluid system piping results in more limiting environmental conditions than the break in proximate high-energy fluid system piping, the provisions of 2.B(iii) should be applied.
- (v) Fluid Systems Qualifying as High-Energy or Moderate-Energy Systems. Through-wall leakage cracks instead of breaks may be postulated in the piping

of those fluid systems<sup>5</sup> that qualify as high-energy fluid systems for only a short operational period but qualify as moderate-energy fluid systems for the major operational period.

C. Type of Breaks and Leakage Cracks in Fluid System Piping

(i) Circumferential Pipe Breaks

The following circumferential breaks should be postulated individually in high-energy fluid system piping at the locations specified in 2.A of this position:

- (1) Circumferential breaks should be postulated in fluid system piping and branch runs exceeding a nominal pipe size of 1 inch, except where the maximum stress range<sup>2</sup> exceeds the limits specified in 2.A(iii)(1) and 2A(iii)(2), but the circumferential stress range is at least 1.5 times the axial stress range. Instrument lines, as well as 1 inch and less nominal pipe or tubing size, should meet the provisions of Regulatory Guide 1.11.
- (2) Where break locations are selected without the benefit of stress calculations, breaks should be postulated at the piping welds to each fitting, valve, or welded attachment.
- (3) Circumferential breaks should be assumed to result in pipe severance and separation amounting to at least a one-diameter lateral displacement of the ruptured piping sections unless physically limited by piping restraints, structural members, or piping stiffness as may be demonstrated by inelastic limit analysis (e.g., a plastic hinge in the piping is not developed under loading).
- (4) The dynamic force of the jet discharge at the break location should be based on the effective cross-sectional flow area of the pipe and on a calculated fluid pressure as modified by an analytically or experimentally determined thrust coefficient. Limited pipe displacement at the break location, line restrictions, flow limiters, positive pump-controlled flow, and the absence of energy reservoirs may be taken into account, as applicable, in the reduction of jet discharge.
- (5) Pipe whipping should be assumed to occur in the plane defined by the piping geometry and configuration and to initiate pipe movement in the direction of the jet reaction.

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<sup>5</sup> The operational period is considered "short" if the fraction of time that the system operates within the pressure-temperature conditions specified for high-energy fluid systems is about 2% of the time that the system operates as a moderate-energy fluid system (e.g., systems such as the reactor decay heat removal system qualify as moderate-energy fluid systems; however, systems such as auxiliary feedwater systems operated during PWR reactor startup, hot standby, or shutdown qualify as high-energy fluid systems).



(ii) Longitudinal Pipe Breaks

The following longitudinal breaks should be postulated in high-energy fluid system piping at the locations of the circumferential breaks specified in 2C(i):

- (1) Longitudinal breaks in fluid system piping and branch runs should be postulated in nominal pipe sizes 4-inch and larger, except where the maximum stress range<sup>2</sup> exceeds the limits specified in 2.A(iii)(1) and 2.A(iii)(2), but the axial stress range is at least 1.5 times the circumferential stress range.
- (2) Longitudinal breaks need not be postulated at terminal ends.
- (3) Longitudinal breaks should be assumed to result in an axial split without pipe severance. Splits should be oriented (but not concurrently) at two diametrically opposed points on the piping circumference such that the jet reactions cause out-of-plant bending of the piping configuration. Alternatively, a single split may be assumed at the section of highest tensile stress as determined by detailed stress analysis (e.g., finite element analysis).
- (4) The dynamic force of the fluid jet discharge should be based on a circular or elliptical ( $2D \times \frac{1}{2}D$ ) break area equal to the effective cross-sectional flow area of the pipe at the break location and on a calculated fluid pressure modified by an analytically or experimentally determined thrust coefficient as determined for a circumferential break at the same location. Line restrictions, flow limiters, positive pump-controlled flow, and the absence of energy reservoirs may be taken into account, as applicable, in the reduction of jet discharge.
- (5) Piping movement should be assumed to occur in the direction of the jet reaction unless limited by structural members, piping restraints, or piping stiffness as demonstrated by inelastic limit analysis.

(iii) Leakage Cracks

Leakage cracks should be postulated at those axial locations specified in 2.A(v) for high-energy fluid system piping and in those piping systems not exempted in 2.B(iii)(1) for moderate-energy fluid system piping.

- (1) Leakage cracks need not be postulated in 1-inch and smaller piping.
- (2) For high-energy fluid system piping, the leakage cracks should be postulated to be in those circumferential locations that result in the most severe environmental consequences. For moderate-energy fluid system piping, see 2.B(iii)(2).
- (3) Fluid flow from a leakage crack should be based on a circular opening of area equal to that of a rectangle one-half pipe diameter in length and one-half pipe wall thickness in width.
- (4) The flow from the leakage crack should be assumed to result in an environment that wets all unprotected components within the

compartment, with consequent flooding in the compartment and communicating compartments. Flooding effects should be determined on the basis of a conservatively estimated time period necessary to effect corrective actions.

### **C. REFERENCES**

- A. 10 CFR Part 50, Appendix A, General Design Criterion 4, "Environmental and Dynamic Effects Design Bases."
- B. American Society of Mechanical Engineers. Boiler and Pressure Vessel Code, Section III, "Rules for Construction on Nuclear Power Plant Components," and XI, "Rules for Inservice Inspection of Nuclear Power Plant Components." New York, NY American Society of Mechanical Engineers.
- C. Regulatory Guide 1.11, "Instrument Lines Penetrating Primary Reactor Containment."
- D. U.S. Nuclear Regulatory Commission. SECY-93-087, "Policy, Technical, and Licensing Issues Pertaining to Evolutionary and Advanced Light-Water Reactor (ALWR) Designs," Washington, DC. April 2, 1993; SRM-93-087 issued on July 21, 1993.

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#### **PAPERWORK REDUCTION ACT STATEMENT**

The information collections contained in the Standard Review Plan are covered by the requirements of 10 CFR Part 50 and 10 CFR Part 52, and were approved by the Office of Management and Budget, approval number 3150-0011 and 3150-0151.

#### **PUBLIC PROTECTION NOTIFICATION**

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